

A Novel Approach for Internal Short Circuit Prediction of Lithium-Ion Batteries by Random Forest

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Internal short circuit (ISC) prediction is a critical challenge for battery failure detection (BFD). Accurate ISC prediction can effectively reduce the risk of battery thermal runaway (BTR) and ensure the safe use of lithium-ion batteries (LiB). The battery ISC is difficult to detect in early stages, and it takes a long time to determine the battery ISC via detection of the battery self-discharge phenomenon. Therefore, to achieve a simple and easy-to-use method for rapid measurement, a model for battery ISC prediction realized by the random forest classifier (RFC) is proposed in this paper. According to the relaxation behavior of LiB, sample data of ordinary batteries and batteries in the ISC state are collected by the hybrid pulse power characteristic (HPPC) test. The MATLAB curve fitting tool is used to fit the voltage relaxation curve in the sample data to obtain the parameters of the equivalent circuit model (ECM), and these parameters are used in the construction of the sample feature. Gray relational analysis (GRA) is used to select the features of the sample data, and the hyperparameters of the RFC model are obtained by a grid search (GS) with “Out-of-Bag” (OoB) errors. Through experimental analysis, the effectiveness and accuracy of the proposed method are verified, which is not only beneficial for BFD but also, increases the reliability of battery use.

Keyword: Lithium-ion batteries; Internal short circuit; Random forest classifier; Equivalent circuit model; Gray relational analysis; Grid search

1. INTRODUCTION

Battery ISC is deemed to be one of the main reasons for triggering the thermal runaway of electric vehicles (EVs) [1, 2]. The early stage of the ISC last for a long time, the battery does not have the obvious characteristics of abnormal self-discharge, and the safety risk is low. As soon as the battery ISC enters the later stage, it will have the usual obvious characteristics, the battery terminal voltage will decrease

obviously, and the temperature of the battery will rise sharply. Because there will be heat accumulation in the process of battery ISC, it will trigger the battery heat abuse chain reaction in a short time, leading to the battery heat being out of control. Even if ISC only happens to the battery, it is likely to cause a series of accidents and even large LiB fires [3]. Since the time interval between the later stage of battery ISC and the thermal runaway of the battery is very short, there is almost no safety and time allowance for the prediction of the later stage of ISC to take corresponding measures. In contrast, there will be a sufficient safety and time margin if battery ISC is detected in the early stage to take corresponding countermeasures to solve the battery ISC problem ahead of time.

1.1. Review of prediction approaches

For the ISC prediction of battery packs, Ouyang et al. [4] developed a detection method based on parameter identification of the battery difference model (CDM). Through the analysis of the battery ECM, they found an abnormal open-circuit voltage (OCV) and resistance of the ISC battery. Experimental results show that the OCV difference of the ISC battery will increase gradually. However, under constant current conditions, the method may not be able to effectively determine OCV differences. X Feng et al. [5] studied battery ISC using a three-dimensional (3-D) electrochemical thermal coupling model. The short circuit resistance of the battery may produce too much heat, and excessive heat generated by ISC batteries was modeled. Experimental results show that the state of charging (SoC) of the ISC battery is abnormal [2]. Through internal and external experiments on LiB, R Zhao et al. [6] adopted an improved electrochemical thermal model (ETM) to predict the temperature change of the battery. Z Chen et al. [7] proposed a fault diagnosis method based on the online model. Although progress has been made in these studies, there is a heavy computational burden to identify model parameters in engineering applications.

Several experimental methods have been used for battery ISC prediction. Nail penetration is a common method of determining battery health [8, 9]. Christopher D.Rahn devised a nail made up of sensors, used to gather experimental data with battery ISC [10]. Wang Hsin Wang designed an improved kneading torsion test method by increasing the torque on battery ISC [11]. Extrusion testing is another method and is the use of round rods or hard plates to press batteries to monitor ISC [12, 13]. The cell diaphragm may be broken by shear stress during crushing tests, or experiments may lead to contact between positive and negative components. The methods for nail penetration and crushing are easy to test, but it's difficult to control the progress of ISC experiments, mainly because the contact area and the short layer are difficult to control. As a key ISC parameter, the short circuit resistance of the battery is largely determined by the contact area [14]. To conquer this challenge, Premanand Ramadass used a hole compression way to trigger a battery ISC [15]. Donal P.Finegan [16] used PCM material instead of pores on the battery partition. When the battery is heated to a specific temperature, the wax will melt, which causes the battery cathode material and negative electrode material to come into contact. Although these experimental methods are easy to implement, they are hard to hold. In addition, putting metal particles into a battery or reassembling the battery may affect battery performance.

Battery ISC can cause the battery temperature to rise. Chen et al. construct an electrothermal coupling model to further research the temperature distribution of ISC batteries [17]. Feng et al. designed

an electrothermal coupling model to reveal the corresponding relationship between the temperature and ISC state of LiBs [18]. Zhang et al. studied the relationship between battery ISC and mechanical abuse to analyze the corresponding battery temperature rise [19]. The results show that the temperature distribution of the battery pack is uneven. As a result, temperature-dependent prediction methods can be influenced by battery thermal management or the battery ISC external environment.

The battery ISC reaction mechanism is complex and difficult to obtain. Additionally, there are some other battery ISC prediction methods. Through the use of X-ray technology, Sun et al. observed lithium dendrite growth and deformation of the battery diaphragm during the ISC process [20]. Rui Guo, et al. also used X-ray technology to study the process of battery thermal runaway and ISC triggers to improve the safety of battery design [21]. Guo et al. studied the whole battery ISC process by overdischarging the battery SoC to -100% [22]. Xiangdong Kong, et al. have established a pseudo two-dimensional model of a micro ISCr battery [23], revealing the battery drain phenomenon and the change of battery parameters when micro ISCr occurs in the battery, and also found that the electrical conductivity of the separator is the key parameter describing ISCr. Furthermore, through simulation and experiments, it is found that the impedance of the micro ISCr battery is different from that of the normal battery. Dongsheng Ren, et al. study on the relationship between battery ISC and thermal runaway [24]. Lishuo Liu, et al. comparative study of battery ISC alternative triggering methods [25].

Chemical reactions, heat accumulation, temperature increases and so on accompany battery ISCs. Therefore, a model-based battery ISC prediction method needs to establish a battery thermal model, electrochemical model, and ISC model [4-7]. However, in engineering applications, such methods usually require a heavy computational burden to identify the model parameters. ISC states in batteries are triggered by experimental techniques, such as nail penetration, extrusion testing, and reassembly of the battery. Experimental methods for ISC prediction of these batteries [8-16], which are usually easy to operate but difficult to control and reproduce, may bring about serious safety incidents, such as thermal runaway. There are two main factors that challenge temperature-based methods [17-19]: the temperature distribution on the surface of the battery is uneven, and the surface temperature of the battery is easily affected by the environment. Although some progress has been made in existing research on ISC prediction, there is still a lack of simple and effective methods for the early prediction of battery ISC. At the early stage of battery ISC, the short circuit current is small, the short circuit scale is relatively small, and the Joule effect heat from the short circuit current is also very small. In addition to the heat dissipation design of the battery, there is little heat dissipation in the early stage of the ISC. Moreover, the battery SoC or OCV changes relatively slowly due to the low short circuit current. Hence, it is difficult to detect ISC at an early stage by thermal or conventional voltage methods, and developing a simple and effective fast prediction method for battery ISC is a meaningful and challenging task.

1.2. Contribution and organization

To overcome such challenges, a model implemented by RFC is proposed for LiB ISC prediction. The contributions made in this research are as follows.

(1) A novel method for LiB ISC prediction is proposed. The RFC model only needs a few short-term data samples and can work efficiently for rapid measurement, which does not depend on a thermal-electrical coupled model, heavy computational burden, or time-consuming parameter identification.

(2) Based on the relaxation behavior of LiBs, the data samples of the normal battery and battery with the ISC state are acquired by a group of current pulses that last only several minutes. This method for short-term feature acquisition is easy to implement in engineering applications.

The following sections of this article are organized as follows. In Section 2, prior research related to battery ISC is introduced. Section 3 introduces the feature structure and the modeling method of battery ISC prediction. The results and analysis of the battery ISC prediction are introduced in Section 4. Section 5 gives a discussion of battery ISC prediction, and section 6 serves as a conclusion.

2. PRIOR RESEARCH OF BATTERY ISC

2.1. An Introduction of battery ISC

While the positive and negative electrodes inside the battery are switched on, ISC will occur. There are usually four types of ISCs according to the structure of the LiB [26]: aluminum-copper (Al-Cu), copper cathode material (Ca-Cu), aluminum anode material (Al-An) and cathode material (Ca-An). Battery ISCs are caused by three main reasons: mechanical abuse, thermal abuse and electrical abuse.

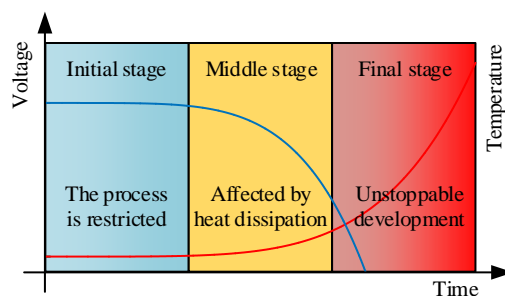


Figure 1. The battery ISC evolution process

The evolution of the battery ISC state includes early, intermediate and final stages [27], as shown in Fig. 1. When the ISC resistance is high in the early stage of ISC, the battery discharge will cause the voltage to decrease slowly. At low exothermic power, the heat generated inside the battery can escape, so the battery temperature will not change significantly. The intermediate stage is the transition stage of the battery ISC. During the final stage of the ISC state, the ISC resistance is small, the current is large, and the battery voltage drops rapidly. The exothermic power of the battery is very large, which will produce a large amount of heat, and the temperature of the battery will rise. Based on the failure temperature of the battery partition, the battery diaphragm will break. As a result, with a large short circuit area between the positive and negative electrodes of the battery, the battery terminal voltage will be reduced to 0 V. In the meantime,

the high temperature will trigger the thermal runaway chain reaction, which will release a lot of heat in a short time, and ultimately trigger the thermal runaway of the battery [28].

2.2. The relaxation characteristics of lithium-ion batteries

During battery testing, charging and discharging the battery will touch off the distribution of electrons and ions in the electrode to be unbalanced. This phenomenon is called battery polarization [29]. Because of this phenomenon, the electrode potential deviates from the equilibrium potential. Generally, there are three main types of battery polarization [30]. First, because of the resistance of the electrodes, electrolytes, and partitions, the voltage will drop, which is the ohmic polarization of the battery. Second, charge transfer is associated with the lithium ions of the battery and is known as battery activation polarization. Finally, concentration polarization is determined by the lithium-ion in solid-phase diffusion.

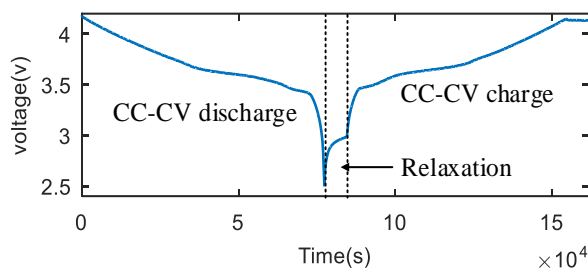


Figure 2. The relaxation process of the battery during testing

When the battery stops charging and discharging, the battery voltage is still unstable during the relaxation time, as shown in Fig. 2, which can be regarded as the depolarization process of the battery. Fig. 3 shows in the relaxation curve of an LiB, where the battery voltage is first discharged at a current rate of 1 C to reduce the battery voltage to 3.3 V, and then the discharge is stopped to enter the relaxation time. The battery voltage rises sharply from the cutoff voltage V_0 to the final stage of the battery discharge V_1 , caused by the rapid response and redistribution of the battery depolarization. The stage from V_1 to V_2 is the process of cell activation and concentration depolarization. The cell voltage rises rapidly from the initial state and then slowly tends to stabilize, which is determined by the charge balance in the particle-electrolyte interface and the particle body.

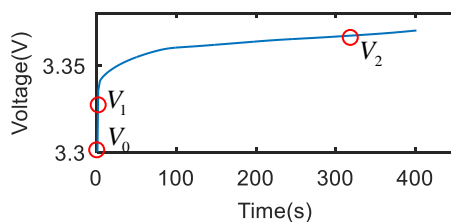


Figure 3. The relaxation curves of battery voltage

2.3. Problem formulation of battery ISC

The voltage response of the battery test will be normal when ISC does not occur. However, when battery ISC occurs, the characteristics of lithium-ion migration inside the battery will change, which will affect the polarization phenomenon of the battery, thus affecting the battery voltage response process. Hence, the battery ISC problem can be transformed into a two-class problem to address. Emphasis is placed on selecting appropriate models and providing data samples to ensure accurate battery ISC prediction. Therefore, the data set for model training can be represented as follows:

$$\Psi = \{X, Y\} \tag{1}$$

where $X = \{x_1, x_2, \dots, x_n\}$ and $Y = \{y_1, y_2, \dots, y_n\}$ are the input sample data and output results, respectively. Here, $x_k = [F_1(k), F_2(k), F_3(k), F_4(k), F_5(k)]$ and $y_k = \{1, -1\}$, where $F_1(k)$, $F_2(k)$, $F_3(k)$, $F_4(k)$, $F_5(k)$ are the sample features of the battery test, 1 and -1 are sample labels indicating whether the battery is exhibiting ISC or not.

2.4. The parameter identification of battery ECM

In general, the battery dynamic behavior can be described by an ECM composed of several resistance and capacitance (RC) combinations, as shown in Fig. 4, which is a second-order RC battery ECM.

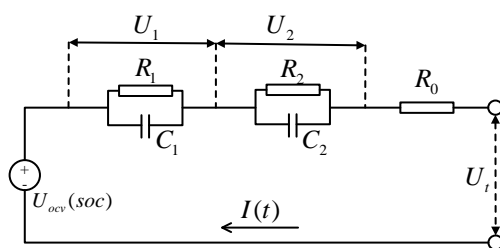


Figure 4. A second-order battery ECM

The battery ECM is composed of three parts: U_{ocv} , the ohmic resistance (R_0), and two RC equivalent circuits for polarization. The parameters U_0 , U_1 , U_2 , and U_t are the ohmic overpotential, diffusion overpotential, charge transfer overpotential, and battery terminal voltage, respectively.

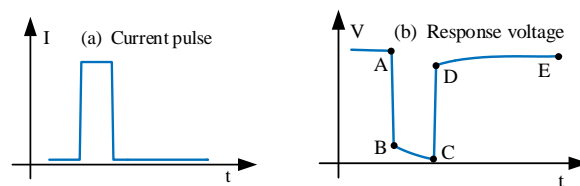


Figure 5. The impulse discharge response of an LiB

According to Kirchoff's law, the circuit equation can be written as:

$$\begin{cases} \dot{U}_1 = -\frac{1}{R_1 C_1} U_1 + \frac{1}{C_1} I \\ \dot{U}_2 = -\frac{1}{R_2 C_2} U_2 + \frac{1}{C_2} I \\ U_t = U_{ocv} - U_1 - U_2 - IR_0 \end{cases} \quad (2)$$

According to the second-order battery ECM and Fig. 5, the formula for calculating R_0 is as follows:

$$R_0 = \frac{|U_D - U_C|}{I} \quad (3)$$

According to Fig. 5, in the stage from A to C, the RC circuit is in the zero state response, and the voltage in this area can be obtained by:

$$U_t(t) = U_{ocv}(t) - IR_0 - IR_1(1 - e^{-t/\tau_1}) - IR_2(1 - e^{-t/\tau_2}) \quad (4)$$

where $\tau_1 = R_1 C_1$, $\tau_2 = R_2 C_2$.

In the stage from C to E, the RC circuit is in the zero input state, and the battery voltage during the process of D to E is:

$$\begin{aligned} U_t(t) &= U_{ocv}(t) - U_1(t) - U_2(t) \\ &= U_{ocv}(t) - U_{10}e^{-t/\tau_1} - U_{20}e^{-t/\tau_2} \end{aligned} \quad (5)$$

where U_{10} , and U_{20} are the initial values of the battery transient voltage.

By the MATLAB curve fitting tool, the coefficients of the above formula can be obtained, and the parameters of the battery model can be obtained as follows:

$$R_1 = \frac{U_{10}}{I}, R_2 = \frac{U_{20}}{I}, C_1 = \frac{I\tau_1}{U_{10}}, C_2 = \frac{I\tau_2}{U_{20}} \quad (6)$$

3. MODELING AND METHODOLOGY

3.1. Feature construction

According to the polarization phenomenon, the voltage relaxation curve can be obtained during the battery test. Hence, the response voltage data (including charging and discharging data) collected using HPPC test methods are used to construct the features. The test result is shown in Fig. 6. Fig. 6(a) is the current pulse, Fig. 6(b) is the voltage response, and Fig. 6(c) is the voltage relaxation curve.

The hybrid pulse current was discharged at a current rate of 1 C and charged at a current rate of 1 C during the battery HPPC test, followed by current rates of 2 C and 3 C, respectively. The duration of the current pulse in Fig. 6(a) is 10 s, the relaxation time is 30 s, and the amplitudes are 1 C, 2 C and 3 C. Moreover, there is a relaxation time after each pulse charge and discharge. The battery response voltage diagram in Fig. 6(b) can be obtained by HPPC in the battery pulse test, and the voltage relaxation curve diagram in Fig. 6(c) can then be acquired from the charge and discharge response voltage.

The battery ECM parameters R_0 , R_1 , C_1 , R_2 , and C_2 can then be obtained by the MATLAB curve fitting tool to fit the relaxation curve, and from which the characteristics F1-F5 can be extracted, as described in Section 2.4. The reason for choosing this curve to construct the feature is the relaxation curve is obtained when the battery state is stable, which can ensure the accuracy of the constructed features. Moreover, Ouyang et al. proposed a battery pack ISC detection method by identifying the battery differential model parameters in the literature [4]. By analyzing of the battery ECM model, they found that the OCV and resistance of the ISC battery were abnormal. Therefore, according to the relaxation curve in the open-circuit state of the battery, the parameters of the battery ECM model are fitted, and the features of the data samples are constructed.

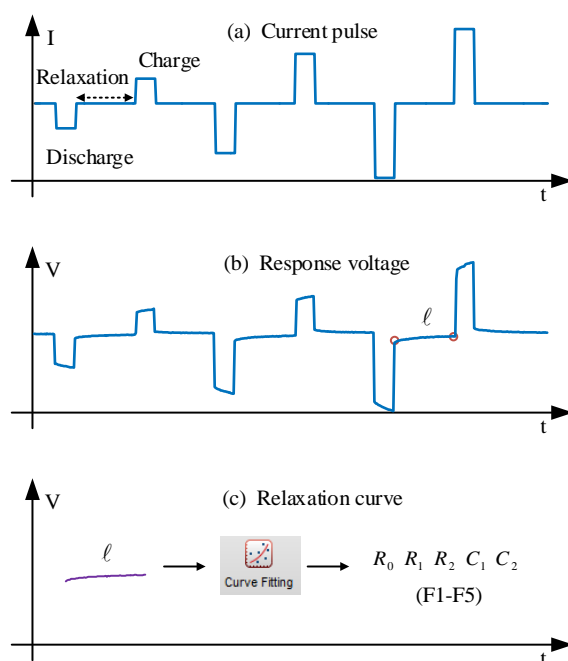


Figure 6. The schematic of the current pulse test

3.2. Features extraction

Feature selection has a large influence on the performance of the machine learning (ML) model, but continuously increasing the features of the model will not accordingly improve the performance of the model. Of course, the final performance of the model depends largely on the number of features and their construction methods. Therefore, to study the relationship between sample features and battery ISC, grey correlation analysis (GRA) is used for complete feature selection [31]. Based on grey system theory, the relationship degree is measured according to the similarity between factors. Hence, GRA supplies a quantitative measure of system evolution and is suitable for dynamic process analysis (DPA). The calculation process is as follows:

(1): The reference sequence $Y = \{y(k) | k = 1, 2, \dots, n\}$ is constructed, where $y(k) = ISC(k)$, the comparative sequence $X_i = \{x_i(k)\}$, here $X_i = F_i$;

(2): The data is preprocessed;

(3): The relational coefficients are calculated:

$$\xi_i(k) = \frac{\min_i \max_k |y(k) - x_i(k)| + \rho \max_i \max_k |y(k) - x_i(k)|}{|y(k) - x_i(k)| + \rho \max_i \max_k |y(k) - x_i(k)|} \quad (7)$$

where ρ is the identification coefficient, $\rho \in (0, 1)$

(4): The relational grade r is calculated:

$$r_i = \text{mean}(\sum_{i=1}^n \xi_i(k)) \quad (8)$$

Redundant items may exist in the selected sample features, but the features obtained after the correlation grade calculation will not affect the final battery ISC prediction results. The relationship between the obtained sample features and the battery ISC according to the calculation steps of the above GRA is shown in Table 1. When the value of the relation grade is equal to 1.0, the relationship degree is the largest. Therefore, there is a high correlation between the extracted sample features and battery ISC, which indicates that feature selection can ensure that the RFC model can accurately predict battery ISC state.

Table 1. The relational between features F_i and SoH

Feature	F1	F2	F3	F4	F5
Grades	0.8255	0.8032	0.7962	0.8238	0.8216

3.3. ISC prediction by RFC

Breiman proposed the random forest (RF) algorithm in 2001[32]. The RF model generates a large number of decision trees (DTs) that pose as regression or classification tools, and the output of the RF is the mean of the output of all of the DTs. In a nonparametric model, DTs are still named classification and regression trees (CARTs), which is a statistical model developed by Breiman et al. [33]. Each DT constituted by a decision node and a leaf node. The decision node evaluates the sample of each input through the test function and then passes it to variety branches according to the sample characteristics. In the process of learning, the DT grows based on the sample data.

Let X be an input vector with m features, and Y be an output scalar. Then, the training set including n observations can be revealed as follows:

$$S_n = \{(x_1, y_1), (x_2, y_2), \dots, (x_n, y_n)\}, X \in R^m, Y \in R \quad (9)$$

In the process of model training, the input data fed to the model are split at each node, so the parameters of the split function need to be optimized to fit the data set S_n . In the first step, the decision tree should be optimally split, where the splitting process will start from the root node, each node obtains new input data, and then this step is repeated until the terminal leaf is hit. Finally, when the maximum

number of levels is reached, the growth of the tree should be stopped, and a estimation function $\hat{h}(X, S_n)$ is realized based on the data set S_n .

The random forest classifier (RFC) is an extension of CART technology. Each tree in the RF will randomly grow a subset of estimators, and the RF will construct multiple unrelated DT during the training process. The RF uses the basic classifier $h(X, \Theta_k)$ with an L-tree structure, where Θ_k is a set of autocephaly and uniformly distributed random vectors. The RFC model is an integrated method that combines all generated DTs through bagging or bootstrap aggregation algorithms (BAAs). This technique is able to use with lots of regression methods to reduce the variance associated with predictions. The process of RF randomly collecting samples is called the boot procedure, which is acquired by randomly selecting n observation values from the data set S_n and replacing them, and the probability of each observation value being selected is $1/n$. To construct a set $\hat{h}_1(X, S_n^{\Theta 1}), \dots, \hat{h}_q(X, S_n^{\Theta q})$ of q prediction trees, the definition is as shown in the following formula, and a bagging algorithm is used to select multiple bootstrap samples $(S_n^{\Theta 1}, \dots, S_n^{\Theta q})$.

$$\hat{Y}_i = \hat{h}_i(X, S_n^{\Theta i}) \tag{10}$$

where $i=1, \dots, q$. The integration generates q outputs corresponding to each tree, and the aggregation is carried out by averaging the outputs of all of the DTs. Therefore, the output estimated value Y can be gained by the following formula:

$$\hat{Y} = \text{sgn}\left(\sum_{l=1}^q \hat{Y}_l = \frac{1}{q} \sum_{l=1}^q \hat{h}(X, S_n^{\Theta l})\right) \quad l=1, 2, \dots, q \tag{11}$$

where \hat{Y} is the output of the l -th tree, $l=1, 2, \dots, q$. The skeleton of the RFC model for ISC prediction is shown in the figure below.

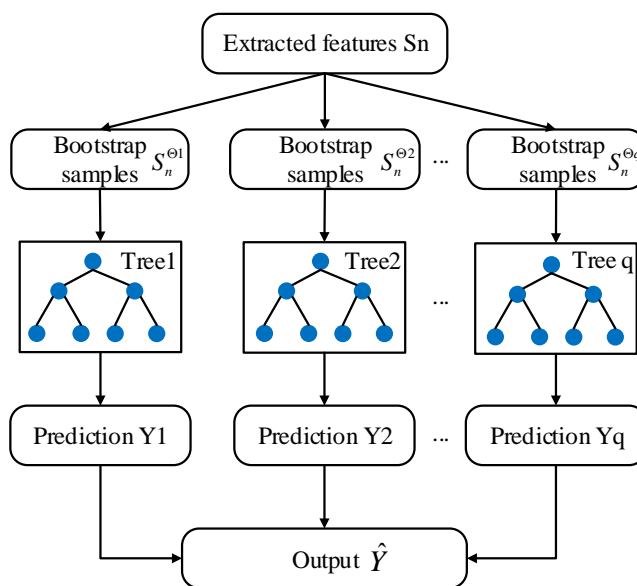


Figure 7. Schematic diagram of the RFC model for battery ISC prediction

3.4. Hyperparameter optimization of RFC model

Ensemble learning is currently a very popular class of machine learning (ML) methods that conforms the modeling results of whole models by construct several models on datasets. RF is composed of randomly generated DT and is a representative integration algorithm. By integrating multiple weak classifiers, the overall model has higher accuracy and better generalization performance. A distinctive advantage of the RF is the using of “out-of-bag” (OoB) data to estimate the generalization error. In the construction of DTs, random back extraction is used.

The OoB is a data set that is not adopted in the model training for the current tree. This ensemble estimation of generalization error proposes the precision of the DT classification and at the same time helps to quantify the significance of the sample features. The OoB estimation calculates the classification of each sample by the DT when it is an OoB sample. The majority vote is used as the classification result of the data sample. The ratio of the number of misclassifications to the whole number of samples is introduced as the OoB misclassification rate of the RF. The RF generalization error of an unbiased estimate is able to evaluate internally, in other words, the error of an unbiased estimate can be established during the generation process.

The basic theory of the GS method is to divide the grid over a specific range, and use the value of the optimal number of DTs and the number of leaves of the RF tree to traverse all points in the network. Combined with the OoB error method, the accuracy of the model classification can be verified by the training set under this parameter value. Finally, the most accurate parameters are determined as the best model parameters.

4. ANALYSIS OF EXPERIMENTAL

This section introduces the experimental analysis, which includes data description and collection, training and testing of the RFC model, verification and results of the RFC model.

4.1. Data description

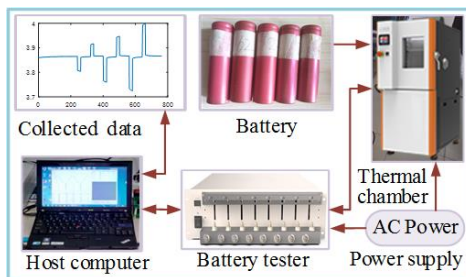


Figure 8. The experimental setup of the test platform

The experimental platform for battery testing and data acquisition is shown in Fig. 8. The test platform consists of an LiB, temperature control box, battery test system and user test computer. After

the battery is placed in the temperature control box, the battery test system is connected by the temperature control box, and the battery test system is connected with the power supply and PC. Finally, the computer obtains the test data to complete the battery test experiment. The 18650 LiB used in the experiment has a cycle life between 1000 and 1500 cycles. Other relevant parameters of the battery are listed in Table 2.

For normal battery samples, the battery aging test and HPPC test are as described in section 3. The battery sample data collection process is as follows: after the battery aging test, the battery sample data are collected using the HPPC test at 5%, 10%, 15%, 20%, and 25% depth of discharge (DoD). In the test experiment, the sampling time was set to 1 second, a total of 12 batteries were tested, and a total of 60 data samples were collected for model training. For batteries in the ISC state, a total of 5 battery samples were tested. The data were collected 12 times, each time according to the HPPC method. A total of 60 samples of batteries in the ISC state were collected. In the data sample, three random samplings (20/each time) were performed, and 3 test sets were constructed for model verification.

Table 2. Cell parameters

Brand name	Battery weight	Nominal capacity	Nominal voltage	Charge/discharge cutoff voltage
Sanyo	45 g	2.4 Ah	3.7 V	4.2 V/3.0 V

4.2. Model training

The experiment was performed in Windows 8.0 by MATLAB 2015 and MATLAB TreeBagger [34]. In order to prevent multiple dimensions of raw sample data from affecting model training, data preprocessing must be performed to dispel this effect, and then improve the convergence rate during model training. In this paper, the minimum-maximum normalization method is used, as shown below.

$$x' = (x - \min_x) / (\max_x - \min_x) \quad (12)$$

where x and x' are the raw data value and scaled data value, respectively, and \max_x and \min_x are the maximum and minimum values of the sample, respectively.

The adaptive assessment plays an essential role. In this paper, the OoB error method on the number of optimal DTs is used to evaluate the performance of RFC models. The RFC model is trained by using different numbers of DTs according to the GS principle, and the corresponding OoB error is obtained. According to the convergence of the OoB error, an optimal number of decision trees are finally selected. The OoB error analysis and convergence diagram of model training is shown in Fig.9.

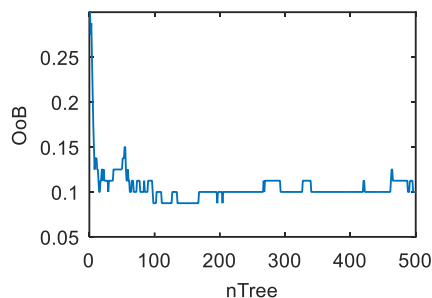


Figure 9. OoB error of RFC model training

According to the above OoB error analysis diagram, it can be concluded that when the number of DTs is near 100, 110, and 120, the training error of the model is the smallest, reaching 0.08. When the number of DTs increases, the accuracy of the model is improved accordingly. However, after more than 100, the OoB error changes very little, and the performance of the model does not improve with the increase in the number of DTs. On the other hand, when the number of DTs increases, the computational overhead is increased. Therefore, the number of DTs selected in this paper is 100. The OoB error can be used as an unbiased estimate of the generalization error of the RFC model, and its results are equivalent to k-fold cross validation (CV). Therefore, the use of the RFC model to predict the battery ISC without CV can ensure that the model has good generalization.

4.3. Performance metrics

To evaluate the prediction performance of the RFC model for battery ISC, three performance metrics are introduced in this paper: prediction precision, recall rate and f-score. The prediction precision is a measure of the accuracy of the identification model to judge the unknown sample as positive. The recall rate is a measure of the accuracy of all positive samples in the data set. Generally, it is difficult to take into account both high precision and high recall rate, so the f-score is adopted to evaluate the precision and recall rate synthetically. The specific definitions of each metric are shown below.

$$precision = \frac{TP}{TP + FP} \quad (13)$$

$$recall = \frac{TP}{TP + FN} \quad (14)$$

$$f\text{-score} = (1 + \beta^2) \frac{precision \times recall}{\beta \times precision + recall} \quad (15)$$

where TP is the number of true positive samples, FP is the number of false-positive samples, TN is the number of true negative samples, and FN is the number of false-negative samples. Parameter β is used to control the weight of the precision and recall rate. In general, the value is equal to 1.0, and the importance of the two metrics is the same.

4.4. Model validation

To verify the comprehensive performance of the RFC model, the model needs to be trained and tested. First, the battery ISC prediction model is trained by the training dataset. Then, three random test sets are used to verify the trained model. For accurate validation of the RFC prediction models, the test data sets used for the models are different from the training data sets.

Table 3. The statistics of the test results for ISC prediction

Test set	precision	recall	f-score
No. 1	0.9646	0.8410	0.9099
No. 2	0.9285	0.7805	0.8481
No. 3	0.9384	0.9384	0.9384
Average	0.9526	0.8533	0.8988

The statistics in the table above show that the RFC model tested on the No. 2 test set produces the worst prediction results, and its precision, recall and f-score are 0.9285, 0.7805 and 0.8481, respectively. The RFC model tested on the No. 3 test set obtained better prediction results. Its precision, recall and f-score were 0.9384, 0.9384 and 0.9384, respectively, which obviously outstrip the prediction accuracy of the test results from the No. 2 test set. The prediction result of the RFC model tested on the No. 1 data set is an ideal test result.

These test results confirmed the comprehensive performance of the RFC model. Although the RFC model tested on dataset No. 2 did not obtain satisfactory prediction results, fortunately, the other two tests both obtained high-precision ISC battery predictions. In particular, for the RFC model, the average value of the prediction results is obtained on the entire test set, showing clearly that the trained model own good robustness and generalization ability. Through the HPPC test method, sample data of the normal battery and the battery with the ISC state are collected. When constructing the sample features, normal and abnormal class sample features can be obtained, which ensures that the classifier can achieve high accuracy.

5. DISCUSSION

5.1. The influence of feature selection on the RFC model

To verify the accuracy of the sample feature selection, five RFC models are trained by the data set without one feature each time, and then three test sets are used to test the models. Table 4 lists the prediction results of each model. When the data set without F2 features is used to train the model, the prediction results are obviously very poor, the average precision is as low as 0.8718, and the average recall rate, and

f-core are 0.9070 and 0.8864, respectively. Moreover, when using a dataset without F3 features to train the model, it will also produce unsatisfactory prediction results. The average values of its ISC prediction precision, recall rate and f-core are 0.9122, 0.8776 and 0.8944, respectively. The remaining three models, that is, the models not trained with F1, F4 and F5 features, produced relatively better prediction results compared with other models, but they were also inferior to the models trained with all five input variables. In short, all of the selected input variables will have an impact on the battery ISC prediction, and are essential for the ISC prediction model.

Table 4. The statistical of test results for ISC estimation

Minus feature	Test set	precision	recall	f-score
F1	Test 1	0.9656	0.8331	0.9053
	Test 2	0.9243	0.7688	0.8395
	Test 3	0.9384	0.9384	0.9384
	Average	0.9512	0.8468	0.8944
F2	Test 1	0.9243	0.8660	0.8942
	Test 2	0.7557	0.9196	0.8297
	Test 3	0.9354	0.9354	0.9354
	Average	0.8718	0.9070	0.8864
F3	Test 1	0.9322	0.8799	0.9053
	Test 2	0.8660	0.8145	0.8395
	Test 3	0.9384	0.9384	0.9384
	Average	0.9122	0.8776	0.8944
F4	Test 1	1.0000	0.8331	0.9053
	Test 2	0.9243	0.7688	0.8395
	Test 3	0.9384	0.9384	0.9384
	Average	0.9512	0.8468	0.8944
F5	Test 1	1.0000	0.8331	0.9053
	Test 2	0.9243	0.7688	0.8395
	Test 3	0.9354	0.9354	0.9354
	Average	0.9402	0.8458	0.8934

5.2. The influence of hyperparameter on the RFC model

The RFC model is very easy to use, and only one parameter needs to be adjusted: the number of DT nTree. The parameter nTree is the number of DTs used in the RFC model, indicating how many sample subsets there are. A larger nTree means that more DTs are used for classification in the RFC model, which easily leads to overfitting. When the value of nTree is smaller, fewer DTs are used for classification in the RFC model, and the model is not easy to fit and may be underfit. Therefore, when the parameter nTree is too large or too small, the generalization ability of the model may not be ideal. As shown in Fig. 10, when nTree is greater than 90, the three indicators of prediction precision, recall rate and f-core tend to stabilize, and the classification accuracy value on test set 1 reaches the maximum value of 100%.

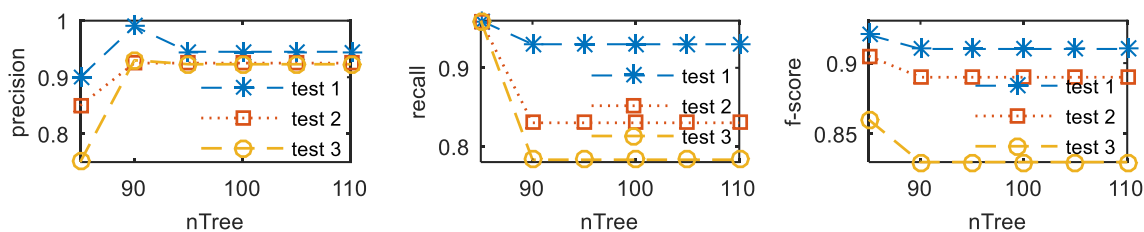


Figure 10. The relationship between the parameter nTree and performance metrics

The optimal number of DT nTree has the greatest impact on the RFC model. Of course, the model has other parameters, but the impact is small. For example, the maximum depth of the DT indicates the maximum depth that the DT can grow when the RFC model is constructed. If set to none, the DT will not control the depth of the subtree when constructing the optimal prediction model. When the model has a large sample size and many features, limiting the maximum depth can be considered to prevent excessive computer overhead. When the model sample size is small, there is no need to limit the maximum depth.

5.3. Comparison with other ISC detection methods

The research is based on symmetrical loop circuit topology to detect the internal short circuit in a battery pack connected in parallel [35]. The internal short circuit is judged based on number theory and circuit topology. The recursive least squares (RLS) algorithm can be used to lock the faulty unit online, and an ISC state with a resistance of less than 10Ω can be detected within 15 s. Another work developed a lumped thermal evolution model (TEM) based on the battery equivalent circuit model (ECM) [36]. An extreme learning machine (ELM) is used to synthesize multiple scattered configuration TEM/ECM submodels to approximate the distribution characteristics of actual batteries. Multiple types of correlation vector machines (RVM) are used to distinguish the battery ISC states. The experimental results verify the reliability of the model structure, the level misjudgment rate is 14.59%, and the state misjudgment rate is as low as 3.13%. In [37], the author proposed an early ISC detection method based on the state of charge (SOC) correlation, which can be used for the online detection of battery ISC under dynamic conditions. The SOC of each battery is estimated through an extended Kalman filter (EKF), and a moving window is used to calculate the correlation coefficients for adjacent batteries to ensure the accuracy and stability of the estimation. Experimental results show that the method is fast and accurate, and can detect the early ISC of 100Ω online under dynamic conditions within 20.4 hours. The research presented in [38] proposes a novel and accurate algorithm based on a model that can detect the soft ISC_r state of the battery online regardless of the load current. The battery equivalent circuit model with ISC_r state is used to extract the open circuit voltage of the battery, thereby obtaining the enhanced relationship between the open circuit voltage and the charging state. The research results show that the relative error of the estimated failure index does not exceed 6.4%. This paper uses the HPPC test method to collect the voltage response curves of normal batteries and ISC state batteries as sample data, and then constructs sample feature variables F1-F5 to train the RFC model. The test precision, average recall rate and f score are 0.9526, 0.8533 and 0.8988, respectively. The experimental results show that this method can achieve high-precision battery ISC

prediction. In the [35], symmetric loop circuit topology is mainly used to detect the battery ISC state. In the [36] and [38], the prediction of the battery ISC state is based on the battery ECM, which is highly dependent on the battery model. In the [37], it is necessary to use the EKF to obtain the battery SOC, which easily increases the estimation error.

6. CONCLUSIONS

The HPPC method is used to test normal batteries and ISC batteries, and the voltage response curve of the batteries is collected as the data sample. Then, the RFC model is trained by the data sample to predict the battery ISC. Based on the above research, the following conclusions can be drawn.

First, the HPPC test method is used to collect the partial voltage response curve as sample data. This nonintrusive and nondamaging method only takes several minutes to complete, and is easy to implement in engineering. The parameters R_0 , R_1 , C_1 , R_2 , and C_2 of the second-order RC battery ECM are acquired by using the MATLAB curve fitting tool to fit the relaxation curve in the sample data, which constitutes the feature variables F1-F5 of the sample. To configure the RFC model, only one parameter, nTree, needs to be tuned, because the other parameters have little effect on the performance of the model. As shown in Fig. 10, when the parameter nTree is greater than 90, the test precision, recall rate, and f-score are stable between 0.8 and 1.0, and the classification accuracy reaches the maximum value of 97.46%. By analyzing the influence of the parameter nTree on the performance of the RFC model, the parameters of the RFC model can be determined. Third, the trained RFC model is verified by the three random test data sets. The average values of the test precision, recall and f-score are 0.9526, 0.8533, and 0.8988, respectively. Experimental results show that this method achieves high-precision battery ISC prediction.

CREDIT AUTHORSHIP CONTRIBUTION STATEMENT

Bin Xiao: Investigation, Methodology, Writing original draft, Writing-review & editing, Validation, Formal analysis. Bing Xiao: Project administration, Supervision, Validation.

DECLARATION OF COMPETING INTEREST

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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References

1. C. J. Orendorff, E. P. Roth, and G. Nagasubramanian, *J. Power Sources*, 15(2011) 6554.
2. N. Williard, W. He, C. Hendricks, and M. Pecht, *Energies*, 6(2013) 4682.
3. Aircraft incident report: auxiliary power unit battery fire. Japan airlines Boeing 787, JA 829J,

- Boston, Massachusetts, January 7, 2013. National Transportation Safety Board, DC. Rep no. PB2014-108867, 2014.
4. M. G. Ouyang, M. X. Zhang, X. N. Feng, L. G. Lu, J. Q. Li, X. M. He, Y. J. Zheng, *J. Power Sources*, 294(2015)272
 5. X. N. Feng, C. H. Weng, M. G. Ouyang, and J. Sun, *Appl. Energy*, 161(2016)168
 6. R. Zhao, J. Liu, and J. J. Gu, *Appl. Energy*, 173(2016) 29.
 7. Z. Y. Chen, R. Xiong, J. P. Tian, X. Shang, and J. H. Lu, *Appl. Energy*, 184(2016) 365.
 8. G. Z. Liang, Y. M. Zhang, Q. Han, Z. P. Liu, Z. Jiang, S. Tian, *J. Power Sources*, 342 (2017) 836.
 9. Y. D. Zhu, F. W. Yan, J. Q. Kang, C. Q. Du, *Int. J. Electrochem. Sci.*, 12(2017) 6895.
 10. T. R. Tanim, M. Garg, C. D. Rahn, *Proceedings of the ASME 2016 Power and Energy Conference*, Charlotte, North Carolina, USA
 11. H. Wang, E. Lara-Curzio, E. T. Rule, C. S. Winchester, *J. Power Sources*, 342(2017) 913.
 12. J. Zheng, Y. Xu, X. Gao, J. Zheng, H. He, Z. Li, *Int. J. Electrochem. Sci.*, 12(2018) 11620
 13. H. Wang, A. Kumar, S. Simunovic, S. Allu, S. Kalnaus, J. A. Turner, J. C. Helmers, E. T. Rules, C. S. Winchester, P. Gorney, *J. Power Sources*, 341 (2017) 156.
 14. R. Zhao, J. Liu, J. J. Gu, *Energy*, 123 (2017) 392.
 15. P. Ramadass, W. F. Fang, Z. M. Zhang, *J. Power Sources*, 248 (2014) 769.
 16. D. P. Finegan, E. Darcy, M. Keyser, B. Tjaden, T. M. M. Heenan, R. Jervis, J. J. Bailey, R. Malik, N. T. Vo, O. V. Magdysyuk, R. Atwood, M. Drakopoulos, M. DiMichiel, A. Rack, G. Hinds, D. J. L. Brett and P. R. Shearing, *Energy Environ. Sci.*, 6(2017) 1377.
 17. M. B. Chen, F. F. Bai, W. J. Song, J. Lv, S. L. Lin, Z. P. Feng, Y. L. Li, Y. L. Ding, *Appl Therm Eng*, 120(2017) 506.
 18. M. B. Chen, F. F. Bai, S. I. Lin, W. J. Song, Y. Li, Z. P. Feng, *Appl. Therm. Eng.*, 146(2019) 775.
 19. C. Zhang, S. Santhanagopalan, M. A. Sprague, A. A. Pesaran, *J. Power Sources*, 2015(290) 102.
 20. F. Sun, R. Moroni, K. Dong, H. Markötter, D. Zhou, A. Hilger, L. Zielke, R. Zengerle, S. Thiele, J. Banhart, and I. Manke, *ACS Energy Lett*, 2(2017) 94.
 21. R. Guo, L. G. Lu, M. G. Ouyang, X. N. Feng, *Sci. Rep.*, 6(2016) 30248.
 22. R. Guo, L. G. Lu, M. G. Ouyang, X. N. Feng, *Sci Rep*, 6(2016) 30248.
 23. X. D. Kong, G. L. Plett, M. S. Trimboli, Z. D. Zhang, D. D. Qiao, T. Z. Zhao, Y. J. Zheng, *J. Storage Mater.*, 27(2020) 101085.
 24. D. S. Ren, X. N. Feng, L. S. Liu, H. J. Hsu, L. G. Lu, L. Wang, X. M. He, M. G. Ouyang, *Energy Storage Mater*, 34(2021) 563.
 25. L. S. Liu, X. N. Feng, M. X. Zhang, L. G. Lu, X. B. Han, X. M. He, M. G. Ouyang, *Appl. Energy*, 259(2020) 114143.
 26. S. Santhanagopalan, P. Ramadass, J. Zhang, *J. Power Sources*, 1(2009): 550.
 27. X. N. Feng, M. G. Ouyang, X. Liu, L. G. Lu, Y. Xia, X. M. He, *Energy Storage Mater.*, 10(2018) 246.
 28. X. N. Feng, M. Fang, X. M. He, M. G. Ouyang, L. G. Lu, H. Wang, M. X. Zhang, *J. Power Sources*, 255(2014) 294.
 29. J. C. Jiang, Q. J. Liu, C. P. Zhang, W. G. Zhang, *IEEE Trans. Ind. Electron.*, 12(2014) 6844
 30. P. D. Weidman, D. Ahn, R. Raj, *J. Power Sources*, 249 (2014) 219.
 31. N. Tosun, *Int. J. Adv. Manuf. Technol.*, 28(2006) 450.
 32. L. Breiman, *Machine Learning*, 45(2001) 5.
 33. L. Breiman, J. Friedman, C. J. Stone, R. A. Olshen, 1984, *Chapman and Hall/CRC Press*.
 34. Matlab. Available: <https://www.mathworks.com/products/matlab.html>
 35. Y. Pan, X. N. Feng, M. X. Zhang, X. B. Han, L. G. Lu, M. G. Ouyang, *J. Cleaner Prod.*, 255(2020) 120277.
 36. J. L. Xie, L. Zhang, T. Q. Yao, Z. C. Li, *J. Storage Mater*, 32(2020) 101957.
 37. X. Lai, W. Yi, X. D. Kong, X. B. Han, L. Zhou, T. Sun, Y. J. Zheng, *J. Storage Mater*, 30(2020) 101514.

38. M. Seo, M. J. Park, Y. B. Song, S. W. Kim, *IEEE Access*, 8(2020) 70947.

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