

Influence of Lanthanum and Barium on the Electrochemical Properties of Grid Alloys in Lead-Acid Energy Storage Batteries

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Lead acid battery is the most preferential option for energy storage application because of its mature manufacturing technology, reliability and high safety. Nonetheless, a negative trait is that the lead–calcium (Pb–Ca) alloy may suffer severe corrosion as a result of long-term depth discharge. Herein, corrosion resistance property has been implemented by cyclic voltammetry (CV) approach and the concentration of Pb^{2+} in the mixture solution (acetic acid, nitric acid and hydrogen peroxide) are measured for the first time by inductively coupled plasma atomic emission spectrometry (ICP-AES) after corrosion test. The addition of the lanthanum (La) and barium (Ba) can improve the corrosion resistance of Pb–Ca–Sn–Al alloy in sulfuric acid electrolyte. Furthermore, the outstandingly high conductivity of the oxidation film on aforementioned alloy electrode is achieved because the growth of PbO in the oxidation film is inhibited by the La or Ba in Pb–Ca–Sn–Al alloy. Meanwhile, the addition of La or Ba can improve oxygen evolution performance of alloy electrodes in sulfuric acid electrolyte.

Keywords: Lead alloys; Anodic films; Lead acid battery; Energy storage application

1. INTRODUCTION

To meet the requirement of energy consumption over the world, design and fabrication of energy storage devices with high-performance materials have to be employed [1, 2]. Lead acid batteries are the most preferential option for energy storage application because of their mature manufacturing technology, reliability and high safety [3, 4]. As one of the critical parts of lead acid battery, positive plate grids can affect the performances of resistance and lifetime. At present, the Pb–Ca alloy is the most commonly grid material in lead acid batteries [5, 6]. This alloy material is

especially useful for the maintenance-free type lead acid battery, because it enables the small self-discharge and lower water consumption to be realized [7-9]. However, an undesirable characteristic is that the Pb–Ca alloy may suffer deterioration due to long-term depth discharge: 1) rapid corrosion of the positive grids in energy storage systems; 2) passive film with high impedance characteristics easily formed between the positive grid and the positive active material (PAM).

To address the issues of rapid corrosion of the positive grids, numerous studies have been conducted to excavate advanced grid alloys with elaborate structure and property. The most effective strategy is to involve additives, such as Ag [10, 11], Ba [12, 13], C [14], into lead–calcium alloys and improve mechanical properties, corrosion characteristic in sulfuric acid solution. The addition of Ag in Pb–Sb alloy inhibits the growth of high impedance passivation films. [10]. Pb alloys adding Ba show a better performance in mechanical and corrosion resistance properties [11]. Both graphene and graphite as carbon materials have the properties of improving the corrosion and electrochemical properties of metal composites and are not involved in the electrochemical process [13]. However, in those researches, there are two principal issues have not yet attracted sufficient attention. Firstly, the corrosion behavior of lead alloys was studied by galvanostatic or potentiostatic polarization in those work. But the potential and current density of lead alloys is constantly changing in charge and discharge process of factual operation condition. This means that the corrosion and electrochemical characteristics are not analyzed accurately by galvanostatic or potentiostatic polarization. Secondly, the corrosion resistance is evaluated by mass loss rate or by analysis of lead ions (Pb^{2+}) in sulfuric acid electrolyte after corrosion test. For gravimetric tests, however, a high error in the measurement of the weights of grid alloys would imply a great error in the calculation of corrosion products. Additionally, the corrosion resistance cannot be expressed by the concentration of Pb^{2+} in the sulfuric acid solution because only a small amount of Pb^{2+} gets into the electrolyte in the process of corrosion testing. So it is necessary to research the corrosion characteristics of the grid accurately during the operation of the lead acid batteries.

The crucial issue is typically known as premature capacity loss (PCL), it is due to the high impedance corrosion film (about $10^{10} \Omega \text{ cm}^2$) inevitably formed between the positive grid and PAM. The undesirable composition in this corrosion film is PbO , which has an adverse effect of leading to the high impedance of the positive electrode after use or storage for a certain period of time, therefore, the cycling performance of lead acid battery degrades drastically [15–18]. In order to resolve the problem of PCL, The researchers used various additives to improve the electrochemical performance of anodic film. Metal elements including Ce [19-21], Y [9], La [22, 23], Sm [9, 24, 25], Li [26], Te [27], have been involved into grid materials. It has been show that these metal elements can effectively improve the conductivity of anodic film, and the cycling performance of the lead acid battery. As we all know, positive grid alloys may be subjected to great potential cycles in the process of actual use, the corrosion layer formed at changing potentials can affect the electrochemical properties of the positive grid, and then it may affect the cycling performance of the lead acid batteries. However, the corrosion layer in above investigations are mainly formed on the lead alloys at different constant potentials, and there is fewer articles reveal the metal additives effect on the anodic films formed at the potential cycle corresponding to energy storage application.

To address the challenges further, cyclic voltammetry (CV), a type of potentiodynamic electrochemical measurement, has been used to reveal the formation of corrosion film in the factual operation through the certain potential cycle of grid alloys. The influences of La and Ba on the corrosion behaviors at potential cycle and conductivity of corrosion film have been investigated in this paper.

2. EXPERIMENTAL

2.1 Sample preparation

The alloys was prepared by fused heavy mixtures of pure lead (99.99 wt.%), pure calcium (99.99 wt.%), pure tin (99.99 wt.%), aluminum(99.90%), lead-(1.00 wt.%) lanthanum alloy and lead-(1.00 wt.%) barium alloy in an electric furnace equipped with high temperature alumina crucible at 800 °C for 20 min, an argon gas atmosphere covers on the surface of molten metals to prevent the oxidation of alloys. The molten lead was made into the bulk (20 mm × 20 mm× 400 mm) sample. The content of La and Ba in the Pb–(0.10 wt.%)Ca–(1.10 wt.%)Sn–(0.02 wt.%)Al–La/Ba alloys is listed in Table 1. The samples were manufactured into a form of bulk (1 mm × 1 mm× 0.5 mm). As the working surface, a 1 mm² end surface was abraded with 2000 grit SiC paper, polished with 0.5 μm Al₂O₃ powder successively, and then cleaned using double-distilled water, while others were sealed with epoxy resin. Fig.1 shows the schematic diagram of working electrodes.

2.2 Corrosion tests

The corrosion test was carried out by cyclic voltammetry (CV) from 0.85 V to 1.25 V (vs. Hg/Hg₂SO₄) with a scanning rate of 0.02 mV s⁻¹ in 1.28g cm⁻³ H₂SO₄ solution. After 100 cycles, the corrosion products of working electrode for each alloy was dissolved using 100ml acetic acid solution (20%) and 100ml mixture of nitric acid (20%) and hydrogen peroxide (20%) subsequently, was added to the acetic acid solution. and diluted to a final volume of 1000 ml. The concentration of Pb²⁺ was analyzed using inductively coupled plasma atomic emission spectrometry (ICP-AES).

Table 1. Composition of the cast alloys

Alloys	Mass content fraction (wt.%)	
	La	Ba
Pb-Ca-Sn-Al	0	0
Pb-Ca-Sn-Al-La-1	0.05	0
Pb-Ca-Sn-Al-La-2	0.10	0
Pb-Ca-Sn-Al-La-3	0.15	0
Pb-Ca-Sn-Al-La-4	0.20	0
Pb-Ca-Sn-Al-Ba-1	0	0.05

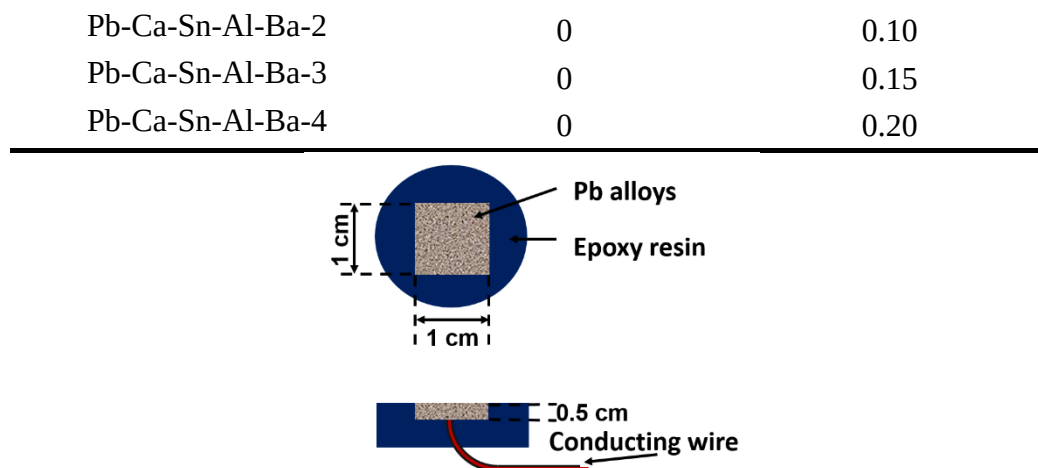


Figure 1. The schematic diagram of working electrodes

2.3 Electrochemical experiments[20]

A conventional three-electrode electrochemical cell was used, the counter electrode was a carbon plate, and all potentials were measured against an $\text{Hg}/\text{Hg}_2\text{SO}_4$ reference electrode. All the electrochemical experiments were performed at CHI660e electrochemical working station. Before experiment, a cathodic polarization at a potential of -1.2 V (vs. $\text{Hg}/\text{Hg}_2\text{SO}_4$) for 20 min was carried out in order to remove any oxidation products formed by aerial.

For Mott–Schottky(M-S) plot, the scanning potential range was from 0.6 V to 1.8 V (vs. $\text{Hg}/\text{Hg}_2\text{SO}_4$) with a scanning rate of 50 mV/s, the measured frequency was 1000 Hz. For electrochemical impedance spectroscopy (EIS), the sweeping frequency was from 1000 kHz to 10 mHz, and the measured potential was 0.9 V (vs. $\text{Hg}/\text{Hg}_2\text{SO}_4$). The photocurrent measurement was made of a conventional three electrode cell of 1-multi neck flash with a quartz window as a photon inlet, a 300 W Xenon arc lamp was used as a light source, a monochromatic light with a wavelength from 200 nm to 800 nm was provided by a scanning digital monochromator controlled by a stepping motor at a scan rate of 5 nm/s, the applied potential was $+0.3$ V, auxiliary focusing lenses were used to raise the intensity of photons toward the monochromator. Linear sweeping voltammetry (LSV) measurement was from 0.8 V to 1.8 V (vs. $\text{Hg}/\text{Hg}_2\text{SO}_4$) with a scanning rate of 10 mV/s.

2.4 Scanning electron microscopy (SEM) measurements

Morphology and elemental analysis of the surface and section of polarized electrodes were determined using SEM (Hitachi S-3400N) techniques equipped with an energy dispersive spectrometer (EDS).

3. RESULTS AND DISCUSSION

For lead acid energy storage battery, the performance of deep cycle mode is a serious problem. This is due to the formation of corrosion products on the surface of the grid alloy. For the sake of evaluation of deep cycling performance for Pb-Ca-Sn-Al-La/Ba alloys, the corrosion test is carried out by CV method. The potential of positive electrode (battery type: HEL500, Shoto Group Co. Ltd.) at 100% state of charge and 100% state of discharge are measured, the results are shown in Table 2. The potential of positive electrode at 100% state of charge (1.25V) and 100% state of discharge (0.85V) are used as the high potential and low potential in CV test, respectively. Fig. 2 shows the CV of Pb-Ca-Sn-Al-La/Ba alloy electrodes performed between 0.85V and 1.25 V with a sweep rate of 0.02 mV s⁻¹ in 1.28 g cm⁻³ H₂SO₄ solution. It can be seen that the CV of nine electrodes display similar features. In the scanning process, two peaks can be observed at about 1.25 V and 1.03V, respectively. The peak at about 1.25 V is associated with the generation of PbO₂ and oxygen release. In the process of cathodic polarization scan, the peak at about 1.03 V indicates the conversion of PbO₂ into PbSO₄.

Table 2. The potential of positive electrode at 100% state of charge and 100% state of discharge

Battery type: HEL500		No.1	No.2	No.3	No.4	No.5
Potential of positive electrode (V/vs. Hg/Hg ₂ SO ₄)	100% state of charge	1.268	1.244	1.265	1.242	1.244
	Average	1.253				
	100% state of discharge	0.845	0.846	0.864	0.849	0.864
	Average	0.854				

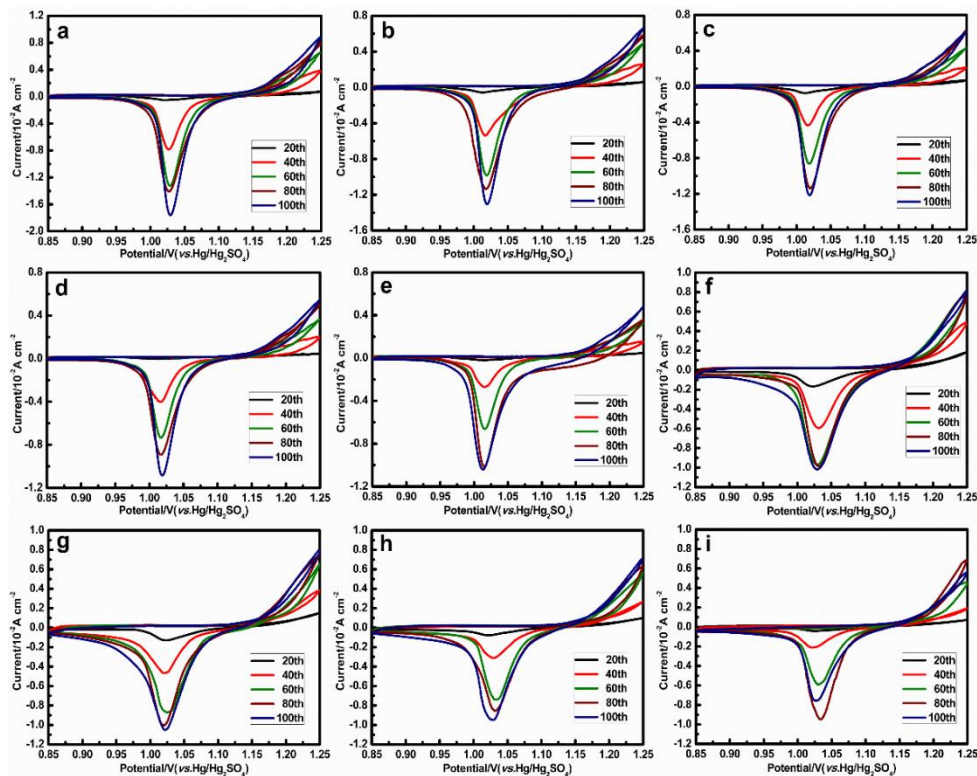


Figure 2. CV for the Pb-Ca-Sn-Al-La/Ba alloy electrodes in $1.28 \text{ g cm}^{-3} \text{ H}_2\text{SO}_4$ solution: a. 0wt.%La; b. 0.05wt.%La; c. 0.10wt.%La; d. 0.15wt.%La; e. 0.20wt.%La; f. 0.05wt.%Ba; g. 0.10wt.%Ba; h. 0.15wt.%Ba; i. 0.20wt.%Ba.

The current densities of peaks at about 1.25 V decrease with the increment of La and Ba content in Pb-Ca-Sn-Al alloy, indicating the increased corrosion resistance of Pb-Ca-Sn-Al alloy [7, 9].

The concentration of Pb^{2+} in the mixture solution (acetic acid, nitric acid and hydrogen peroxide) are measured by ICP-AES, after the corrosion test is completed, and the results are illustrated in Fig.3. The specimens of La-added alloys show substantially lower Pb^{2+} concentration compared to the aforementioned traditional Pb-Ca-Sn-Al alloy, as well as the Ba-added counterparts. In particular, the Pb-Ca-Sn-Al-La-3 alloy shows lowest Pb^{2+} concentration of 61.07 mg L^{-1} , therefore, this alloy demonstrate excellent corrosion resistance property.

In order to specify the impact of La on the corrosion property of Pb-Ca-Sn-Al alloy in H_2SO_4 solution, surface morphology of alloys after corrosion test are shown in Fig.4a-e. Evidently, the morphology of the corrosion products on those electrodes are different, the surface of Pb-Ca-Sn-Al alloy after corrosion test appears some corrosion holes and cracks. The holes and cracks can make the ions (including H^+ , H_2O and SO_4^{2-}) easily pass through the anodic film on Pb-Ca-Sn-Al alloy [9], and then the corrosion rate of the alloy increases. However, this phenomenon has been greatly improved with the addition of La. In addition, it can be seen that the anodic film on alloy electrodes are consisted of amorphous and crystalline products, Fig.4f and g are the EDS analysis for the amorphous and crystalline particles in the Pb-Ca-Sn-Al-La-1 alloys, respectively. Table 3 listed the EDS results of Pb-Ca-Sn-Al-La-1 alloys. From the data of Table 3, the results indicated that the anodic film on alloy electrodes are consisted of PbSO_4 and PbO_{1+x} ($0 \leq x \leq 1$), that is to say, for the corrosion films on Pb-Ca-Sn-Al-La alloys, the distinctive system of $\text{Pb}/\text{PbO}_{1+x}/\text{PbSO}_4$ is formed.

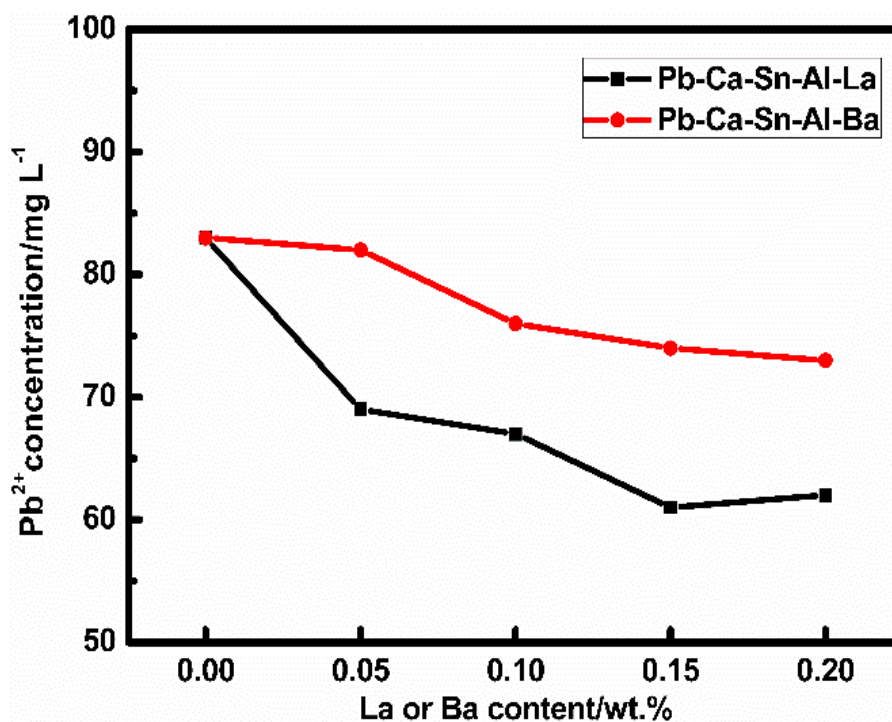


Figure 3. Pb²⁺ concentration of all alloys after corrosion test.

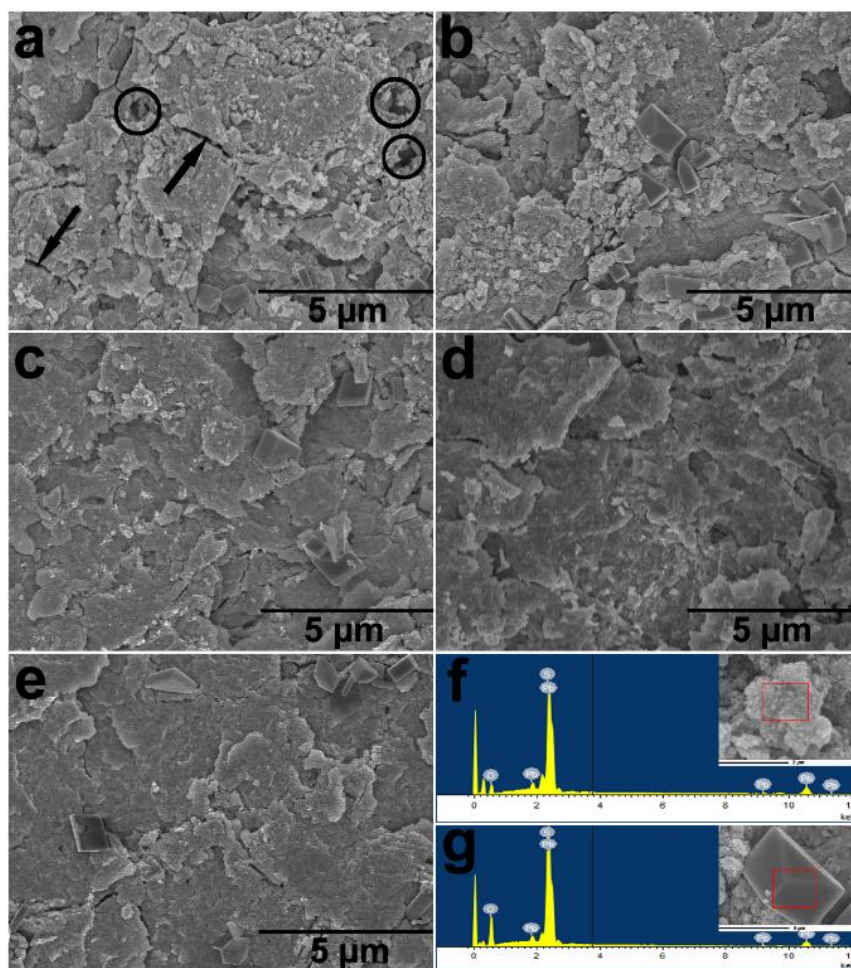


Figure 4. The SEM images of alloys after corrosion test (a.0wt.%La; b.0.05wt.%La; c.0.10wt.%La; d.0.15wt.%La; e.0.20 wt.%La); EDS analysis of amorphous(f) and crystalline products(g).

Table 3. The EDS results of Pb-Ca-Sn-Al-1 alloys

Elements	Atomic percentage/%	
	Figure 4f	Figure 4g
Pb	43.87	16.41
O	58.72	67.23
S	-2.58	16.36

To analyse the impact of Ba on the corrosion resistance of Pb-Ca-Sn-Al alloy in H_2SO_4 solution, the SEM images of corrosion products after corrosion test are shown in Fig.5. It shows that anodic films display the rough and inhomogeneous character similarly. Some corrosion holes and cracks appears on the Pb-Ca-Sn-Al-Ba-1 alloy. As Ba content continues to increase, the cracks on the corrosion film vanished. Compare with Fig.4b-e, $PbSO_4$ particles significantly decreases on the anodic film.

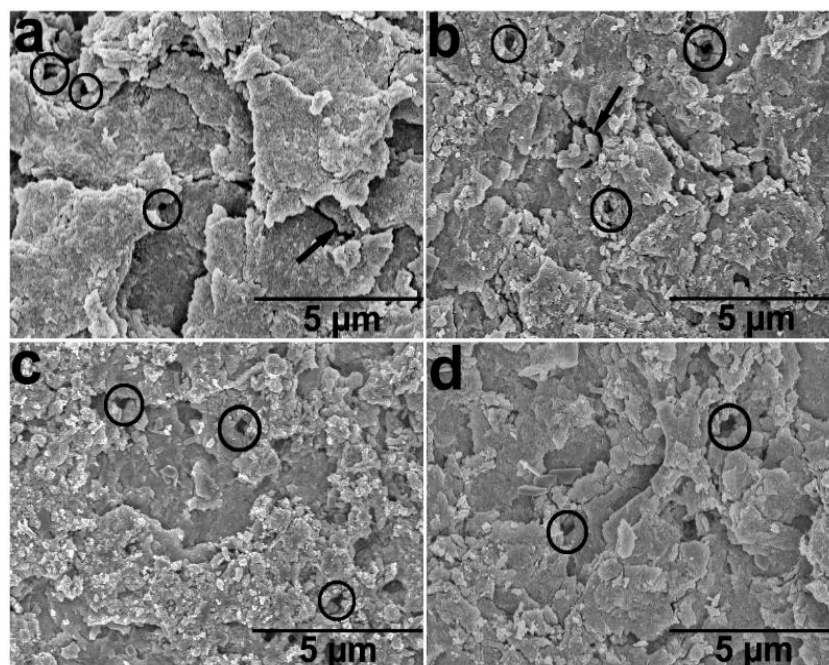


Figure 5. The SEM images of alloys after corrosion test (a. 0.05wt.%Ba; b.0.10wt.%Ba; c.0.15wt.%Ba; d.0.20wt.%Ba) contents after corrosion test.

Mott–Schottky (M-S) measurement is widely used to examine the electronic property of the passive film formed on metal or alloy by measuring the electrode capacitance (C) as a function of the potential (E) [20]. The potential dependence of the C of a semiconductor electrode under depletion layer can be expressed here (for n-type semiconductor) [28-30]:

$$C^{-2} = C_{sc}^{-2} = \frac{2}{\epsilon \epsilon_0 e N_D} \left(E - E_{FB} - \frac{KT}{e} \right) \quad (1)$$

ϵ —the dielectric constant of the passive film; ϵ_0 —the vacuum permittivity ($8.854 \times 10^{-14} \text{ F cm}^{-1}$); e —the electron charge; N_D —the donor density; E_{FB} —the flat-band potential; K —the Boltzmann constant; T —the absolute temperature. N_D can be estimated from the slope of linear fitted M-S plots, while E_{FB} comes from the extrapolation for $C_{sc}^{-2} = 0$ [9, 20, 30].

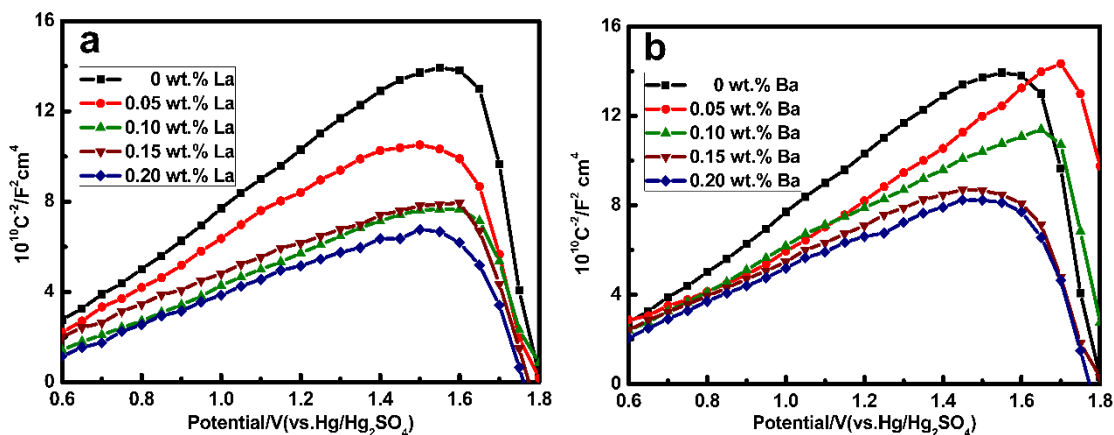


Figure 6. M–S plots of anodic films formed on Pb–Ca–Sn–Al–La/Ba alloys with different La (a) and Ba (b).

Table 4. The slopes of M–S plots of the anodic films on Pb–Ca–Sn–Al–La/Ba alloys

Alloys	slopes
Pb–Ca–Sn–Al	13.10
Pb–Ca–Sn–Al–0.05wt.%La	9.83
Pb–Ca–Sn–Al–0.10wt.%La	7.16
Pb–Ca–Sn–Al–0.15wt.%La	6.56
Pb–Ca–Sn–Al–0.20wt.%La	6.28
Pb–Ca–Sn–Al–0.05wt.%Ba	11.74
Pb–Ca–Sn–Al–0.10wt.%Ba	8.34
Pb–Ca–Sn–Al–0.15wt.%Ba	7.59
Pb–Ca–Sn–Al–0.20wt.%Ba	6.70

The M–S plots of the corrosion products on Pb–Ca–Sn–Al–La/Ba alloys after corrosion test in $1.28 \text{ g cm}^{-3} \text{ H}_2\text{SO}_4$ solution are depicted in Fig.6. Results indicate that there is a significant linear correlation between potential and C^{-2} from 0.6 V to 1.5 V(vs. $\text{Hg}/\text{Hg}_2\text{SO}_4$), meanwhile, the slopes of M–S curves display positive. It shows that the corrosion films on Pb–Ca–Sn–Al–La/Ba alloys have the characteristics of n-type semi-conductors. As shown in Table 4, the slopes of M–S curve have a

tendency to decline obviously with the increment of La or Ba-doping content. According to Eq. (1), the donor density of the corrosion film increases gradually with the increment of La or Ba content, which indicating the increased number of point defect in the corrosion film [9, 30]. The increased point defects density will benefit the conductivity of corrosion films and so much so that the long-term depth discharge performance of the lead acid energy storage battery improved because the point defect in the anodic films can act as the charge carrier.

For the in situ anodic films formed the surface of metals and alloys, photo-electrochemical analysis is an effective analysis often used to investigate their semi-conductive properties. Fig.7 shows the variation of photocurrent and the wavelength of incident light with +300 mV applied potential [9, 30]. It can be seen that the photocurrent has a tendency to increase obviously with increasing the wavelength, when the wavelength of incident light is less than 350nm. The maximum of the photocurrent appears when the incident wavelength arrives at about 350 nm, then the photocurrent decreases with continuing to increase wavelength. Meanwhile, the results indicate that the photocurrent intensity increases with the addition of La or Ba. The point defect within the anodic film can serve as the charge carrier, the electron jumps over the bandgap and passes into the conduction band of the corrosion film, and then the photocurrent occurs. The increasing photocurrent demonstrates the increment of point defect density in the anodic film, it is in agreement with the result of M-S plot [9, 30].

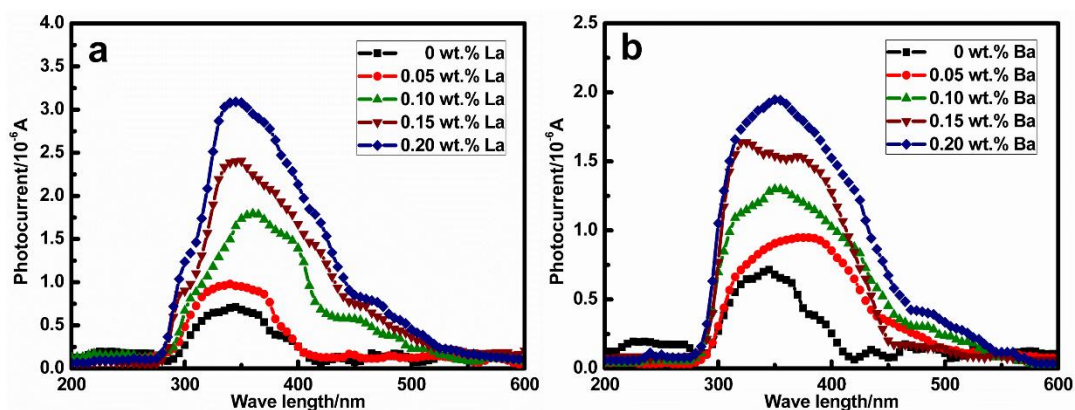


Figure 7. The photocurrent verse wave length plot of the anodic films on Pb-Ca-Sn-Al alloys with different La (a) and Ba (b).

EIS is employed to further studies on the electrochemical properties of corrosion products formed on the Pb-Ca-Sn-Al-La/Ba alloys. Fig.8 showed that the Nyquist plots of the corrosion products formed in the corrosion test on the Pb-Ca-Sn-Al-La/Ba alloys. In the Nyquist plots, the diameter of the depressed semicircle in the high-to-medium-frequency region corresponds to charge transfer resistance, while the sloping line in the low frequency region is assigned to Warburg impedance [20, 31]. The equivalent electron circuit showed in Fig.9 is used to fit the impedance spectra. As showed in Fig.9, R_1 is the solution resistance, R_2 is related to the transfer resistance, Q_1 represents the capacitance of the double layer, R_3 and Q_2 are the resistance and capacitance of the anodic film, W is the Warburg impedance. The fitted results are listed in Table 5. It can be seen that the transfer resistance R_2 increases with the increment of La or Ba content, while the value of R_3

decreased. As the potential of 0.9V is in the growth potential region of PbO, the increment of R_2 value indicates the inhibited growth of PbO in the anodic film [30]. The decrement of R_3 imply that the conductivity of the anodic film enhances. The decrement of capacitance Q_2 indicates a more compact anodic film, then it can be concluded that the micro-channel within $\text{PbO}_{1+x}/\text{PbSO}_4$ film decreases with increasing La or Ba content [9]. That means the compact anodic film of Pb-Ca-Sn-Al-La/Ba alloys can protect the substrate lead of the alloys from corrosion by the H_2SO_4 electrolyte [6].

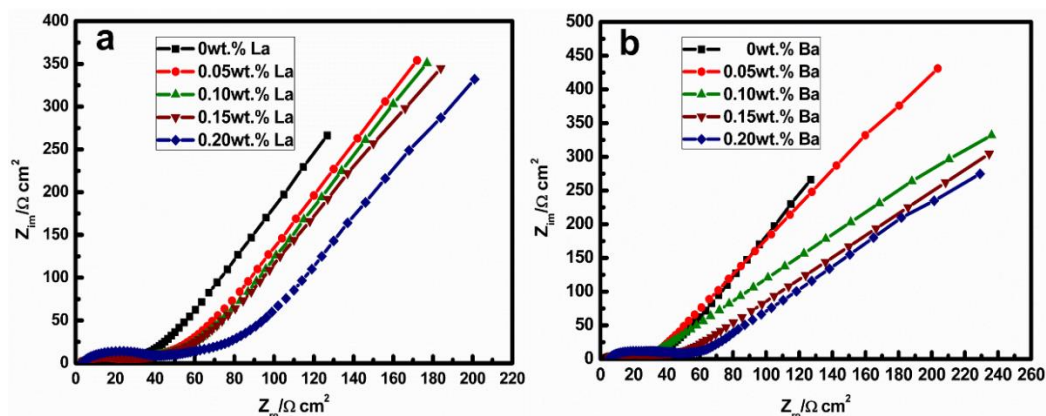


Figure 8. The Nyquist plots of the passive films on the Pb-Ca-Sn-Al alloy electrodes with different amounts of La (a) and Ba (b).

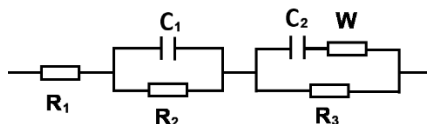


Figure 9. The equivalent electron circuit used to fit the impedance spectra showed in Figure 8.

Table 5. The fitted results of the impedance spectra of the passive films on the Pb-Ca-Sn-Al-La/Ba alloys

Alloys	$R_1/\Omega \text{ cm}^2$	$R_2/\Omega \text{ cm}^2$	$C_1/\text{F cm}^2$	$R_3/\Omega \text{ cm}^2$	$C_2/\text{F cm}^2$	$W/\Omega \text{ s}^{-1/2}$
0wt.%La	4.276	4.63	2.19E-06	14.16	5.71E-05	93.11
0.05wt.%La	4.406	8.50	2.04 E-06	13.06	1.15 E-05	93.38
0.10wt.%La	4.335	8.78	1.97 E-06	12.9	9.38 E-06	100.1
0.15wt.%La	4.053	8.96	1.96 E-06	12.83	8.99 E-06	100.5
0.20wt.%La	3.903	20.83	7.42 E-06	12.04	1.67 E-06	141.2
0.05wt.%Ba	4.798	7.84	1.93 E-06	13.75	1.08 E-05	18.09
0.10wt.%Ba	6.440	9.08	1.41 E-06	13.16	4.25 E-05	82.25
0.15wt.%Ba	5.159	9.89	1.00 E-06	13.01	6.92 E-05	73.40

0.20wt.%Ba	5.889	10.23	7.44 E-07	12.36	1.14 E-05	73.60
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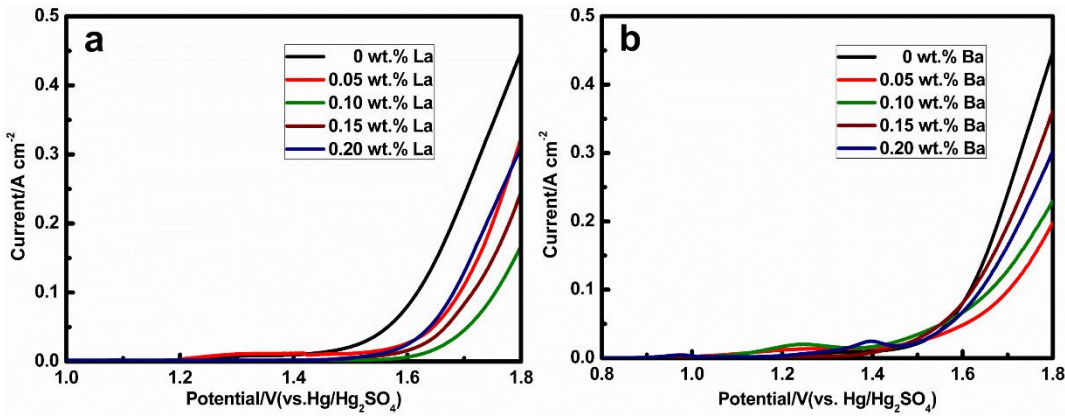


Figure 10. LSV of Pb-Ca-Sn-Al alloy electrodes with different amounts of La (a) and Ba (b) in $1.28 \text{ g cm}^{-3} \text{ H}_2\text{SO}_4$.

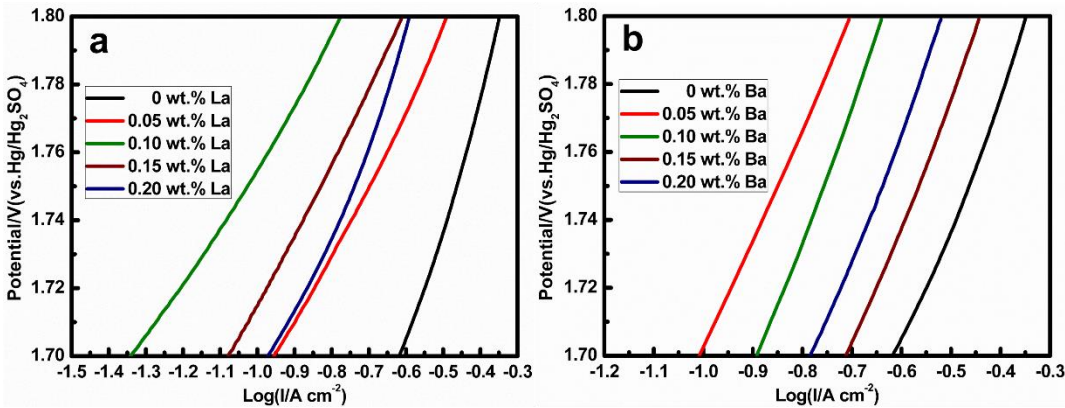


Figure 11. Tafel plots of oxygen evolution on Pb-Ca-Sn-Al alloy electrodes with different amounts of La (a) and Ba (b).

Table 6. Kinetic parameters of the oxygen evolution reaction on Pb-Ca-Sn-Al alloy electrodes with different amounts of La/Ba.

Alloys	a/V	b	R
0wt.%La	1.925	0.372	0.9936
0.05wt.%La	1.900	0.213	0.9970
0.10wt.%La	1.933	0.176	0.9964
0.15wt.%La	1.928	0.214	0.9989
0.20wt.%La	1.928	0.262	0.9857
0.05wt.%Ba	2.028	0.326	0.9998
0.10wt.%Ba	2.049	0.393	0.9992
0.15wt.%Ba	1.960	0.368	0.9989
0.20wt.%Ba	1.992	0.379	0.9942

For the sake of research on the behavior of oxygen evolution of the alloys, the anodic polarization curves were recorded by linear sweep voltammetry (LSV) after corrosion test in 1.28 g cm⁻³ sulfuric acid solution [22]. The LSV results and corresponding Tafel plots are shown in Fig. 10 and Fig. 11, separately. The kinetic parameters of Tafel plots are listed in Table 6. It can be seen that the over potential of oxygen evolution on the Pb-Ca-Sn-Al-La/Ba electrodes is higher than that on Pb-Ca-Sn-Al electrode. It can be seen that the a value of Pb-Ca-Sn-Al-0.10 wt.% Ba alloy is greater than other alloy electrodes. This indicates that the Ba in the alloys effectually relieves the oxygen evolution reaction.

4. CONCLUSIONS

We have demonstrated the deep recycle property of Pb-Ca-Sn-Al-La/Ba alloys that simultaneously addresses the corrosion resistance, conductivity of anodic film, and oxygen evolution issues to promote the properties of the positive grids in lead acid energy storage batteries. Corrosion resistance property has been implemented by CV approach and the concentration of Pb²⁺ in the mixture solution (acetic acid, nitric acid and hydrogen peroxide) are measured by ICP-AES after corrosion test for the first time. The addition of the La and Ba can improve the corrosion resistance of Pb-Ca-Sn-Al alloy and electrochemical property of the anodic films in sulfuric acid solution. Additionally, the addition of La or Ba can decrease the oxygen evolution of alloy electrodes in sulfuric acid. This discovery opens a path for employing multicomponent positive grid materials with rationally designed structures and functions to improve lead acid energy storage batteries.

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